



Specification

TITLE OF INVENTION

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Title: Super Conducting Action Motor (acronym SCAM):

Electrical apparatus for generating a one-directional force, with applications in space vehicle propulsion.

CROSS REFERENCE TO RELATED APPLICATIONS

Not Applicable

STATEMENT REGARDING FEDERALLY SPONSORED RESEARCH OR DEVELOPMENT

Not Applicable

REFERENCE TO A MICROFICHE APPENDIX

Not Applicable

BACKGROUND OF THE INVENTION

This invention pertains to the field of endeavor of electrical (electronic, or non-chemical) space propulsion systems. Within that field of endeavor the invention further

pertains to the exploitation of relativistic electrodynamics and the production of a propulsive force.

DERIVATION OF RELATIVISTIC ELECTRODYNAMIC FORCES ON PARALLEL CONDUCTORS.

This section documents the derivation of equation (i), used as the basis of the force calculations in section DETAILED DESCRIPTION OF THE INVENTION.

The success of the SCAM rests on the equivalence of forces due to magnetic flux analysis and the relativistic effects of charged particles. The framework for this analysis is the classical parallel wire scenario. Without assuming the existence of magnetic flux the forces on the current-carrying wires are shown to satisfy the ampere definition, thus illustrating the equivalence of magnetic flux analysis in the circumstance of relativity^[1]. The approach rests on the hypothesis that positive and negative charges within the wires can be considered separately using a Coulomb force model. Charge invariance is maintained. In calculating the forces, four sets of interaction are considered, namely proton-proton, electron-electron, proton-electron and electron-proton. It is proposed that electron-electron and proton-proton interaction produce forces in accordance with Coulomb, since particle interaction occurs in a single rest frame in each case. However, for interaction of unlike particles, two frames must be used, moving relative to each other, due to the flow of electrons in one wire, moving with respect to the protons in the other wire.

This derivation is a specific mathematical example to show that the study of dynamic charged systems does not require the preconception of magnetic flux. This derivation is consistent with conventional theory^[3].

DERIVATION

Note: if the reader is not interested in mathematics, this derivation, up to equation (i) on page 8, can be skipped without prejudice. The purpose of this derivation is to derive equation (i) relativistically.

Consider the arrangement shown in FIG 14. Two parallel wires L and H , carrying equal currents, are separated in vacuum by a distance a .

λ_{eL} electron density in L

λ_{pL} proton density in L

λ_{eH} electron density in H

λ_{pH} proton density in H

v electron velocity

δl short current segment in L

δh short current segment in H

μ_0 permeability of free space

ϵ_0 permittivity of free space

c velocity of light

The force δF on δh at point h is composed of electrostatic and electrodynamic components:

,

- [1] Electrostatic force in the rest frame of λ_{pL} and λ_{pH} , due to the interaction of $\delta l_{\lambda_{pL}}$

and $\delta h_{\lambda_{pH}}$; this is a repulsive force, hence denoted -ve: $\frac{-\delta l_{\lambda_{pL}} \delta h_{\lambda_{pH}}}{4\pi\epsilon_0 r^2}$.

- [2] Electrostatic force in the rest frame of λ_{eL} and λ_{eH} , due to the interaction of $\delta l_{\lambda_{eL}}$

and $\delta h_{\lambda_{eH}}$; this is a repulsive force, hence denoted -ve: $\frac{-\delta l_{\lambda_{eL}} \delta h_{\lambda_{eH}}}{4\pi\epsilon_0 r^2}$.

- [3] Relativistic electrodynamic force in the rest frame of λ_{pL} , due to the interaction of

$\delta l_{\lambda_{pL}}$ and $\delta h_{\lambda_{eH}}$; this is an attractive force, hence denoted +ve: $\frac{\delta l_{\lambda_{pL}} \delta h_{\lambda_{eH}} \frac{\delta h}{\delta h'}}{4\pi\epsilon_0 r^2}$

where $\delta h'$ is given by the Lorentz length contraction $\delta h' = \delta h \sqrt{1 - \frac{v^2}{c^2}}$. Hence this

force component is $\frac{\delta l_{\lambda_{pL}} \delta h_{\lambda_{eH}}}{4\pi\epsilon_0 r^2 \sqrt{1 - \frac{v^2}{c^2}}}$.

- [4] Relativistic electrodynamic force in the rest frame of λ_{pH} , due to the interaction of

$\delta l_{\lambda_{eL}}$ and $\delta h_{\lambda_{pH}}$; this is an attractive force, hence denoted +ve: $\frac{\delta l_{\lambda_{eL}} \frac{\delta l}{\delta l'} \delta h_{\lambda_{pH}}}{4\pi\epsilon_0 r^2}$.

Similarly, as in case [3], relativistic Lorentz length contraction gives

$\delta l' = \delta l \sqrt{1 - \frac{v^2}{c^2}}$. Hence this force component is $\frac{\delta l_{\lambda_{eL}} \delta h_{\lambda_{pH}}}{4\pi\epsilon_0 r^2 \sqrt{1 - \frac{v^2}{c^2}}}$.

The factors $\frac{\delta h}{\delta h'}$ in [3], and $\frac{\delta l}{\delta l'}$ in [4] are due to the apparent increase in charge density in a moving frame. The velocity v is the electron drift velocity, ie the current through the wire. Then from the viewpoint of the rest frame the length δh contracts to

$$\delta h' = \delta h \sqrt{1 - \frac{v^2}{c^2}}$$

as illustrated in FIG 15. (In FIG 15, the term q denotes the charge in a small length δh . This q is introduced here for illustration only, and is not used generally in the derivation).

The total charge within δh remains unchanged, since charge is invariant under relativistic transformation. However, the length δh itself is not invariant; hence the actual charge $\lambda \delta h$ now appears to occupy a shorter length, $\delta h'$, and so the charge density appears to increase by the factor $\frac{\delta h}{\delta h'}$, ie $\frac{1}{\sqrt{1 - \frac{v^2}{c^2}}}$.

Then the force δF on segment δh is the sum of the forces from [1], [2], [3] and [4]:

$$\delta F = -\frac{\delta l_{pL} \delta h \lambda_{pH}}{4\pi\epsilon_0 r^2} - \frac{\delta l_{eL} \delta h \lambda_{eH}}{4\pi\epsilon_0 r^2} + \frac{\delta l_{pL} \delta h \lambda_{eH}}{4\pi\epsilon_0 r^2 \sqrt{1 - \frac{v^2}{c^2}}} + \frac{\delta l_{eL} \delta h \lambda_{pH}}{4\pi\epsilon_0 r^2 \sqrt{1 - \frac{v^2}{c^2}}}$$

Having derived the force δF in terms of these 4 components, the expression can now be simplified by noting that $\lambda_{pL} = \lambda_{pH}$ and $\lambda_{eL} = \lambda_{eH}$. Also, since attractive and repulsive components were ascribed their appropriate signs in [1], [2], [3] and [4], all the λ terms represent the absolute charge density, so $\lambda_e = \lambda_p$ (for L and H).

These simplifications represent notational changes only; the physical properties are unchanged.

Thus

$$\delta F = \frac{\lambda \lambda}{4\pi\epsilon_0 r^2} \left(-1 - 1 + \frac{1}{\sqrt{1 - \frac{v^2}{c^2}}} + \frac{1}{\sqrt{1 - \frac{v^2}{c^2}}} \right) \delta l \delta h$$

ie

$$\delta F = \frac{2\lambda\lambda}{4\pi\epsilon_0 r^2} \left(-1 + \frac{1}{\sqrt{1 - \frac{v^2}{c^2}}} \right) \delta l \delta h$$

The term $\frac{1}{\sqrt{1 - \frac{v^2}{c^2}}}$ can be re-expressed by the binomial expansion for $(1-x)^{-1/2}$:

$$(1-x)^{-1/2} = 1 + \frac{x}{2} + \frac{3}{8}x^2 + \frac{5}{16}x^3 + \frac{35}{128}x^4 + \frac{63}{256}x^5 + \dots$$

$$(1-x)^{-1/2} = 1 + \frac{x}{2} + \frac{3}{8}x^2 + \frac{5}{16}x^3 + \frac{35}{128}x^4 + \frac{63}{256}x^5 + \dots$$

$$(\text{from } (1+x)^{-1/2} = 1 - \frac{x}{2} + \frac{3}{8}x^2 + \frac{5}{16}x^3 - \frac{35}{128}x^4 - \frac{63}{256}x^5 + \dots)$$

Applying this to the parenthesized term in the expression for δF above,

$$\begin{aligned} -1 + \left(1 - \frac{v^2}{c^2} \right)^{-1/2} &= (1-x)^{-1/2} = -1 + \left(1 + \frac{v^2}{2c^2} + \frac{3}{8} \frac{v^4}{c^4} + \frac{5}{16} \frac{v^6}{c^6} + \frac{35}{128} \frac{v^8}{c^8} + \frac{63}{256} \frac{v^{10}}{c^{10}} + \dots \right) \\ &= \frac{v^2}{2c^2} + \frac{3}{8} \frac{v^4}{c^4} + \frac{5}{16} \frac{v^6}{c^6} + \frac{35}{128} \frac{v^8}{c^8} + \frac{63}{256} \frac{v^{10}}{c^{10}} + \dots \end{aligned}$$

Typically the drift velocity $v \approx 10^{-4} \text{ ms}^{-1}$, so $\frac{v}{c} \approx 10^{-12}$ and $\frac{v^2}{c^2} \approx 10^{-24}$. Hence $\frac{v^2}{2c^2}$

dominates in the expansion above. Using this approximation δF becomes,

$$\delta F \approx \frac{2\lambda\lambda}{4\pi\epsilon_0 r^2} \left(\frac{v^2}{2c^2} \right) \delta l \delta h$$

Given that $c \gg v$, this approximation will now be used in equality form in the continuation of this derivation, with no significant loss of accuracy. Thus δF is expressed as

$$\delta F = \frac{\lambda\lambda}{4\pi\epsilon_0 r^2} \frac{v^2}{c^2} \delta l \delta h$$

This is the attractive force on δh , in the direction of r , due to the equal currents in wire segments δl and δh . The perpendicular force between the wires is $\delta F_x = \delta F \cos \theta$,

where $\cos \theta = \frac{a}{r}$. Therefore $\delta F_x = \frac{\lambda\lambda}{4\pi\epsilon_0 r^2} \frac{v^2}{c^2} \frac{a}{r} \delta l \delta h$

Given this expression for the force attributable to small segments δl and δh on their respective wires L and H , it's now possible to find the total force on wire H by integrating over the interested lengths of the wires over their respective limits.

First, the force on δh due to the entire wire L between limits l_1 and l_2 is simply the integral of δF_x over L . Call this δF_h :

$$\delta F_h = \int_{l_1}^{l_2} \frac{\lambda\lambda}{4\pi\epsilon_0 r^2} \frac{v^2}{c^2} \frac{a}{r} \delta h \delta l$$

The limits in l need to be expressed in terms of position h , since they are measured from δh , situated at point h .

$$\delta F_h = \int_{l_1-h}^{l_2-h} \frac{\lambda\lambda}{4\pi\epsilon_0 r^2} \frac{v^2}{c^2} \delta h \delta l$$

Then the total force on wire H between limits h_1 and h_2 , is the integral of δF_h over H . Call this F :

$$F = \int_{h_1}^{h_2} \int_{l_1-h}^{l_2-h} \frac{\lambda \lambda}{4\pi\epsilon_0 r^2} \frac{v^2}{c^2} \frac{a}{r} \delta l \delta h$$

Substitute in $r^2 = a^2 + l^2$ (from FIG 14):

$$F = \frac{\lambda \lambda}{4\pi\epsilon_0} \int_{h_1}^{h_2} \int_{l_1-h}^{l_2-h} \frac{v^2}{c^2} \frac{1}{a^2 + l^2} \frac{a}{(a^2 + l^2)^{1/2}} \delta l \delta h$$

Simplify,

$$F = \frac{\lambda \lambda v^2}{4\pi\epsilon_0 c^2} \int_{h_1}^{h_2} \int_{l_1-h}^{l_2-h} \frac{a}{(a^2 + l^2)^{3/2}} \delta l \delta h$$

Substitute in $\mu_0 = \frac{1}{\epsilon_0 c^2}$

$$\text{and } I = \lambda v \text{ (from } \lambda = \frac{dq}{dl}, v = \frac{dl}{dt} \Rightarrow \lambda v = \frac{dq}{dl} \frac{dl}{dt} = \frac{dq}{dt} = I \text{)}$$

$$F = \frac{\mu_0 I^2}{4\pi} \int_{h_1}^{h_2} \int_{l_1-h}^{l_2-h} \frac{a}{(a^2 + l^2)^{3/2}} \delta l \delta h$$

The integral over l is soluble with the standard integral $\int \frac{dx}{(a^2 + x^2)^{3/2}} = \frac{x}{a^2(a^2 + x^2)^{1/2}}$

$$F = \frac{\mu_0 I^2}{4\pi} \int_{h_1}^{h_2} \left[\frac{al}{a^2(a^2 + l^2)^{1/2}} \right]_{l_1-h}^{l_2-h} dh$$

Apply the limits:

$$F = \frac{\mu_0 I^2}{4\pi a} \int_{h_1}^{h_2} \frac{l_2 - h}{\{a^2 + (l_2 - h)^2\}^{1/2}} - \frac{l_1 - h}{\{a^2 + (l_1 - h)^2\}^{1/2}} dh$$

This can be integrated using the standard integral:

$$\int \frac{l-x}{\{a^2 + (l-x)^2\}^{1/2}} dx = -\{a^2 + (l-x)^2\}^{1/2}$$

Thus

$$F = \frac{\mu_0 I^2}{4\pi a} \left[-\{a^2 + (l_2 - h)^2\}^{1/2} + \{a^2 + (l_1 - h)^2\}^{1/2} \right]_{h_1}^{h_2}$$

Apply the limits:

$$F = \frac{\mu_0 I^2}{4\pi a} \left[-\{a^2 + (l_2 - h_2)^2\}^{1/2} + \{a^2 + (l_1 - h_2)^2\}^{1/2} + \{a^2 + (l_2 - h_1)^2\}^{1/2} - \{a^2 + (l_1 - h_1)^2\}^{1/2} \right] \quad (i)$$

This is the general form for the force on wire H along length $h_2 - h_1$ caused by the current in wire L along length $l_2 - l_1$. This is equation (i) used as the basis of the force calculations in section DETAILED DESCRIPTION OF THE INVENTION.

To corroborate this form consider equal lengths and alignment of lengths L and H so that $h_1 = l_1$ and $h_2 = l_2$. Then $h_1 - l_1 = 0$, $h_2 - l_2 = 0$ and $h_2 - l_1 = l_2 - h_1 = L$ (say).

Then

$$F = \frac{\mu_0 I^2}{4\pi a} \left[-(a^2)^{1/2} + (a^2 + L^2)^{1/2} + (a^2 + L^2)^{1/2} - (a^2)^{1/2} \right]$$

ie

$$F = \frac{\mu_0 I^2}{2\pi a} \left[(a^2 + L^2)^{1/2} - a \right]$$

and the force per metre is

$$\frac{F}{L} = \frac{\mu_0 I^2}{2\pi a} \left[\frac{(a^2 + L^2)^{1/2}}{L} - \frac{a}{L} \right]$$

For very long L such that $L \gg a$

$$\frac{F}{L} \approx \frac{\mu_0 I^2}{4\pi a} \left[\frac{L}{L} - 0 \right]$$

Finally, for the infinite wire scenario $\frac{L}{L} \rightarrow 1$:

$$\frac{F}{L} = \frac{\mu_0 I^2}{2\pi a} \text{ Hm}^{-1} \text{ A}^2 \text{ m}^{-1}$$

Rationalize the units to force per unit length: $\frac{F}{L} = \frac{\mu_0 I^2}{2\pi a} \text{ Nm}^{-1}$.

Then for $a = 1\text{m}$ and $I = 1\text{A}$,

$$\frac{F}{L} = \frac{\mu_0}{2\pi} = \frac{4\pi \cdot 10^{-7}}{2\pi} = 2 \times 10^{-7} \text{ Nm}^{-1}.$$

This is in accordance with the ampere definition of two “infinitely” long wires each carrying 1A, separated by 1m in vacuum:

The ampere is that steady current which when it is flowing in each of two infinitely long straight parallel wires which have negligible areas of cross-section and are 1 metre apart in vacuum, causes each conductor to exert a force of 2×10^{-7} N on each metre of the other.

REQUIREMENT FOR A DIFFERENT PERSPECTIVE

This derivation demonstrates the equivalence of the relativistic electric force and those derived from magnetic flux. When electronic effects are calculated relativistically they completely describe the forces present in dynamic systems. Magnetism is described in terms of relativistic electronics ^[4].

Note that equation (i) is identical to that derived using electromagnetic analysis. Where relativistic analysis differs is as follows:

- electromagnetic analysis posits that the force on wire H is attributable to its interaction with a magnetic field at wire H caused by a current in wire L.
- relativistic analysis posits that the force on wire H is attributable to its interaction with an event that occurred on wire L some time earlier.

It is this small, but on-zero delay that facilitates the design of the SCAM.

Of course, magnetic analysis is very effective at describing physical systems, and is generally chosen in favor of relativistic electronics for reasons of ease. This is of course sensible, because it would be very difficult to describe engineering systems relativistically, taking account of electrons and currents as described in the preceding pages. The relativistic analysis ^{[1], [3]} described above is equivalent to modern textbook theory^[2].

References

- [1] Albert Einstein, *Annalen der Physic*, xvii, 891, 1905
- [2] John R Lucas & Peter E Hodgeson, *Spacetime and Electromagnetism*, pp 187-206, Oxford University Press, ISBN 0-19-852039-5, 1990
- [3] Leigh Page, *A Derivation of the Fundamental Relations of Electrodynamics from Those of Electrostatics*, American Journal of Science, XXXIV: 57, 1912

- [4] Edward M Purcell, *Electricity and Magnetism*, pp 169-199, McGraw-Hill, ISBN 0-17-004908-4, Second Edition 1985

BRIEF SUMMARY OF INVENTION

The invention is an electrical apparatus for generating a one-directional, propulsive force. This application exploits relativistic electrodynamics in such a way that the analysis would not be possible using conventional electromagnetic theory, although the two theories ^{[1], [2]} are the same.

The device has applications in spacecraft propulsion. Conventional spacecraft propulsion systems operate by jettisoning mass out of the spacecraft in one direction, which results in a reactive force in the opposite direction. Conventional propulsion systems thus have a limited life, determined by the time when all the propellant is exhausted.

The action motor differs from the reaction motor (rocket) in that it is all electric. This gives it a lifespan determined by the longevity of the power supply; which in the case of solar power or atomic power could be measured in decades or centuries. Note that although this device offers revolutionary advantages over conventional propulsion systems, it does not provide something for nothing. The SCAM is an electrical device, and needs an electrical power supply. The power supply is out the scope of this patent.

The device works by virtue of the temporal lag affecting the forces experienced on a current-carrying conductor caused by a current in another conductor some distance away, and parallel to the first. By phasing the currents such that the current in

one wire, L, precedes a similar current in another wire, H, H will perceive a current in L when H itself is conducting, but not contrary-wise, i.e. when L is conducting it perceives no current in H, thus experiencing no force. In the description that follows, "segment 1" refers to the segment of Plate 1 in FIG 3, and "segment 2" refers to the segment of Plate 2 in FIG 3. The timing of electrical current pulses in segment 1 and segment 2 is such that segment 2 experiences an attractive force, and segment 1 experiences no force. The force on segment 2 is due to the arrival of the segment 1 signal simultaneous with a current pulse in segment 2, yielding a force of magnitude given by equation (i). The absence of an attractive force in segment 1 is due to there being no current in segment 1 when the segment 2 signal arrives at segment 1. The sum total of all forces on segment 1 and segment 2 is therefore non-zero. This means that there is a one-directional force on the device as a whole. The small force on these two example current segments is multiplied by arranging many such segment pairs in a two-dimensional grid. Figure 3 shows a single segment pair, and their dimension relationships. FIG 3 also shows the arrangement of the feeder wires, aligned perpendicularly to the plate surface, in order not to interfere with the SCAM force.

BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWINGS

FIG 1: current frequency

Shows the current pulse profile with its 1:3 nature. Shows the pulse width (duration), p , with respect to the plate separation, a .

FIG 2: phasing chart

Shows the phase relationship of the currents in the two plates.

FIG 3: x and z separation of 2 segments, ie segment pair

Shows the dimension relationship of the separation of parallel and aligned segments, in the two plates. This figure shows the two segments of a segment pair, one segment in each plate. The segment pair is also shown with the feeder wires, aligned perpendicularly to the plate surface, in order not to interfere with the SCAM force.

FIG 4: x and z separation of neighboring segments

Shows the dimension relationships of the separation of parallel and displaced segments, in the two plates. This figure shows six segments, three in each plate. This is an overhead view, looking down between the two plates.

FIG 5: x and y separations in a single plate

Shows the dimension relationships of the separation of segments in a single plate. This figure shows twelve segments, in a 3 x 4 array.

FIG 6: z and y separation in two plates

Shows the dimension relationships of the separation of parallel and displaced segments, in the two plates. This figure shows eight segments, four in each plate. This is a side view looking into the plates in the direction of segment alignment: only the ends of the segments are visible (shown as dots).

FIG 7: perspective view of the two plates

Shows the three-dimensional nature of the plate arrangement - no segment detail is included.

FIG 8: close-up perspective view of the two plates and current segments

Shows the three-dimensional nature of the plate arrangement - 9 segments are shown in each plate, each plate having a 3 x 3 array.

FIG 9: **m-n segment distance relationship**

Shows geometric distance from Plate 1 (m,0) to Plate 2 (m,n).

FIG 10: **Force between current-carrying conducting wires**

Shows a theoretical parallel wire arrangement. Used to assist the electrodynamic derivation of the force between two parallel conductors, L and H of arbitrary length.

FIG 11: Plate 1 (0,0) to Plate 2 (m,n) segment distance, B

Line of sight distances used for calculating timing differences.

FIG 12: **Timing differences**

Shows timing differences of signals arriving at neighboring segments.

FIG 13: **Gazette view**

Perspective view of the two plates showing segment arrangement.

FIG 14: **Relativistic force between current-carrying conducting wires**

Used in the derivation of equation (i) for the relativistic forces between conductors

FIG 15 Lorentz length contraction

Shows how charge density is altered under relativistic analysis

DETAILED DESCRIPTION OF THE INVENTION

The SCAM consists of two parallel plates of super-conducting elements mounted in a non-conducting substrate. Current is pulsed through the conducting elements in a

controlled manner to produce forces on one plate, but not on the other. The best way to understand the form and function of the SCAM is to consider it from first principles. Once these principles are understood, the design follows.

Two idealized parallel current-carrying conducting wires experience attractive forces according to electrodynamic form (ie relativistic form) of Coulomb's equation,

$$F = \frac{\mu_0 I^2}{4\pi a} \left[- \left\{ a^2 + (l_2 - h_2)^2 \right\}^{1/2} + \left\{ a^2 + (l_1 - h_2)^2 \right\}^{1/2} + \left\{ a^2 + (l_2 - h_1)^2 \right\}^{1/2} - \left\{ a^2 + (l_1 - h_1)^2 \right\}^{1/2} \right] \quad (i)$$

as illustrated in FIG 10. For the derivation of (i) see section BACKGROUND OF THE INVENTION.

In a steady state condition, with equal current in both segments, the attractive forces are experienced by both wires. However, the signal from wire L takes a finite, non-zero time to reach wire H, that time being a/c , where a is the separation of the two wires and c is the velocity of light, in the relevant medium. This can be used to generate non-symmetric forces in L and H by pulsing current I through them as illustrated in FIG 1 and FIG 2. In FIG 1 and FIG 2 the units are as follows:

p = pulse duration = $T / 3$

T = time of one cycle = $1 / f$

f = drive frequency in Hz

$f = c / (3 a)$ where a = segment length = plate separation in metres

Distance ' a ' is fixed for a particular SCAM, but is flexible to support SCAMs of different scales. Typical values for ' a ' would range from 1 cm to 1 km

For example, if $a = 1$ cm, ie 10^{-2} m, then

$f = 3 \times 10^8 / (3 \times 10^{-2}) = 10^{10}$ Hz, ie 10 GHz

$$T = 1 / 10^{10} = 10^{-10} \text{ seconds, and } p = 10^{-10}/3 \text{ seconds}$$

This is the basic principle of the SCAM. The one-way force is multiplied by using an array of elements, each of length a , optimally separated by gaps of length $(1 - \sqrt{15})a$ parallel to current, and by gaps of length $\sqrt{15}a$ normal to the current. The geometric arrangements are shown in section views in FIGs 4, 5 and 6, and in perspective views in FIGs 8 and 13.

PHYSICAL DESCRIPTION

The SCAM comprises two plates of conducting segments, distance a apart, FIGs 7 and 13. Each conducting segment is of length a , equal to the separation, FIG 3. The two plates are rigidly connected to each other so that they cannot move relative to each other. The separation distance a is fixed for a particular SCAM, but this patent covers designs for any a . A small device might use a separation of $a = 1$ cm. A large space-based device might use a separation of $a = 1$ m (metre) or 1 km. The use of a large separation a facilitates the use of a lower frequency current. This scalability will enable future devices to be built increasingly small as faster pulsing technology becomes available.

- Each plate contains an array of conducting segments mounted in a non-conducting substrate, FIGs 5, 8 and 13.
- The conductors of each plate are pulsed with current I at a frequency dependent on the separation of the plates, FIG 1.
- The currents in the two plates are phased, FIG 2.

- The segment feeder wires are arranged perpendicularly to the plate surface, so as to not interfere with the plate force FIG 3.
- Each plate has M elements in the x direction, and N elements in the y direction.
- M is fixed for a particular SCAM, but this patent covers designs for any M.
- Similarly N is fixed for a particular SCAM, but this patent covers designs for any N.
- Typical devices would use M and N in the order of 100 to 1000. M and N may be equal, but they need not be equal.

MAGNITUDE OF THE FORCE PRODUCED

The net force produced by the SCAM is independent of the size of the separation a (page 19: a cancels); as far as physical dimensions are concerned, the net force depends only on M and N. So for example, a SCAM having $M = N = 100$, $a = 0.1$ metre, will produce the same force as a SCAM having $M = N = 100$, $a = 10$ metres.

The net force on the SCAM is calculated by considering the net force due to each segment in Plate 1 interacting with each segment of Plate 2. I.e. the force due to a single segment is calculated by summing the contributions from its neighboring segments on the opposite plate. The total force on the SCAM is the sum of all the forces on the individual segments.

INDIVIDUAL SEGMENT INTERACTIONS

Nomenclature: in the analysis that follows, the indices m and n are relative cardinal segment displacements in x and y . Index $(0,0)$ in Plate 1 represents the Plate 1 segment under examination (the relative origin). Indexes (m,n) represent neighboring

segments in Plate 2, such that Plate 2 (0,0) is the segment pair companion of Plate 1 (0,0), see FIG 11.

$F_{m,n}$ is the force experienced on Plate 2 (m,n) due to current in Plate 1 (0,0).

From equation (i), the force between any two parallel wires is:

$$F = \frac{\mu_0 I^2}{4\pi a} \left[- \left\{ a^2 + (l_2 - h_2)^2 \right\}^{1/2} + \left\{ a^2 + (l_1 - h_2)^2 \right\}^{1/2} + \left\{ a^2 + (l_2 - h_1)^2 \right\}^{1/2} - \left\{ a^2 + (l_1 - h_1)^2 \right\}^{1/2} \right]$$

Where a is the distance shown in FIG 10. Adapting this for the SCAM, let the perpendicular segment separation be $A = \sqrt{1+15n^2} a$ as in FIG 9:

$$F = \frac{\mu_0 I^2}{4\pi A} \left[- \left\{ A^2 + (l_2 - h_2)^2 \right\}^{1/2} + \left\{ A^2 + (l_1 - h_2)^2 \right\}^{1/2} + \left\{ A^2 + (l_2 - h_1)^2 \right\}^{1/2} - \left\{ A^2 + (l_1 - h_1)^2 \right\}^{1/2} \right]$$

Substitute in values $\mu_0 = 4\pi \times 10^{-7} \text{ Hm}^{-1}$, $l_1 = 0$, $l_2 = a$, $h_1 = m\sqrt{15}a$, $h_2 = m\sqrt{15}a + a$

$$F = \frac{10^{-7} I^2}{A} \left[- \left\{ A^2 + 15m^2 a^2 \right\}^{1/2} + \left\{ A^2 + (ma\sqrt{15} + a)^2 \right\}^{1/2} + \left\{ A^2 + (ma\sqrt{15} - a)^2 \right\}^{1/2} - \left\{ A^2 + 15m^2 a^2 \right\}^{1/2} \right]$$

Substitute in $A^2 = a^2 + n^2 15a^2 = a^2(1 + 15n^2)$

$$F = \frac{10^{-7} I^2}{a\sqrt{1+15n^2}} \left[- \left\{ a^2(1+15n^2) + 15m^2 a^2 \right\}^{1/2} + \left\{ a^2(1+15n^2) + (m\sqrt{15} + 1)^2 a^2 \right\}^{1/2} \right. \\ \left. + \left\{ a^2(1+15n^2) + (m\sqrt{15} - 1)^2 a^2 \right\}^{1/2} - \left\{ a^2(1+15n^2) + 15m^2 a^2 \right\}^{1/2} \right]$$

a cancels

$$F = \frac{10^{-7} I^2}{\sqrt{1+15n^2}} \left[- \left\{ 1+15n^2 + 15m^2 \right\}^{1/2} + \left\{ 1+15n^2 + (m\sqrt{15} + 1)^2 \right\}^{1/2} \right. \\ \left. + \left\{ 1+15n^2 + (m\sqrt{15} - 1)^2 \right\}^{1/2} - \left\{ 1+15n^2 + 15m^2 \right\}^{1/2} \right]$$

collect terms:

$$F = \frac{10^{-7} I^2}{\sqrt{1+15n^2}} \left[-2\{1+15n^2+15m^2\}^{1/2} + \{1+15n^2+(m\sqrt{15}+1)^2\}^{1/2} + \{1+15n^2+(m\sqrt{15}-1)^2\}^{1/2} \right]$$

Segment forces calculated with this equation are shown in Table 1 (over page).

Table 1 Force $F_{m,n}$ / Newtons ($\times 10^2$)

	m = 0	m = 1	m = 2	m = 3	m = 4
n = 0	8.284271E-08	1.657607E-09	2.13321E-10	6.351320E-11	2.683900E-11
n = 1	6.155281E-09	2.343748E-09	6.096187E-10	2.168178E-10	9.800905E-11
n = 2	1.632680E-09	1.178737E-09	5.385352E-10	2.855185E-10	1.499315E-10
n = 3	7.339474E-10	6.279738E-10	4.252823E-10	2.617651E-10	1.601344E-10
n = 4	4.145032E-10	3.787467E-10	2.572741E-10	2.130374E-10	1.472746E-10

To illustrate the plate force, consider a SCAM of size $M \times N = 2 \times 3$, as depicted in the non-shaded cells of Table 1.

Due to symmetry, $F_{\pm m, \pm n} = F_{m,n}$

TIMING DIFFERENCES

The forces in Table 1 need to be adjusted to recognize the partial Plate 1 and Plate 2 forces attributable to timing differences. In the ideal situation, as occurs in segment (m,n) and its four nearest neighbors, the Plate 1 contribution is 0% and the Plate 2 contribution is 100%. This ideal does not extend to the more distant neighbors due to Plate 1 to Plate 2 segment separations not being exact multiples of $(1 + 3J)a$, where J is an integer and a is the plate separation. Timing differences are illustrated in FIG 12, based on the line-of-sight segment distances, B , from FIG 11.

From FIG 11, $B = \sqrt{1 + 15(m^2 + n^2)}a$

Line of sight distances for the unshaded segments of Table 1 are shown below:

Table 2 Line-of-sight distances from Plate 1 (0,0) to Plate 2 (m,n)

	m = 0	m = 1
n = 0	a	4a
n = 1	4a	$\sqrt{15} a = 5.568 a$
n = 2	$\sqrt{61} a = 7.810 a$	$\sqrt{31} a = 8.718 a$

EXPLANATION OF FIG 12:

Time proceeds along the abscissa axis, left to right.

For each segment, (m,n) the current pulses are shown for Plate 1 above, and for Plate 2 below. The thicker bottom line then shows the arrival of the Plate 1 (0,0) signal at Plate 2 (m,n); and the thicker top line shows the arrival of the Plate 2 (m,n) signal at Plate 1 (0,0). The overlap of the Plate 1 (0,0) signal with Plate 2 (m,n) produces an attractive force on Plate 2 which is beneficial to the net force on the SCAM. Contrary-wise, the overlap of the Plate 2 (m,n) signal on Plate 1 (0,0) produces an attractive force on Plate 1 which is detrimental to the SCAM. The time units of FIG 12 are as follows:

p = pulse duration = $T / 3$, T = time of one cycle = $1 / f$, f = drive frequency
in Hz

$f = c / (3 a)$ where a = segment length = plate separation in metres

Distance 'a' is fixed for a particular SCAM, but is flexible to support SCAMs of different scales.

Typical values for 'a' would range from 1 cm to 1 km

For example, if $a = 1$ cm, ie 10^{-2} m, then

$f = 3 \times 10^8 / (3 \times 10^{-2}) = 10^{10}$ Hz, ie 10 GHz

$T = 1 / 10^{10} = 10^{-10}$ seconds, and $p = 10^{-10}/3$ seconds

Note: due to the Plate 2 phase shift of p , the Plate 1 arrival times are delayed (right-shifted) by p

From FIG 12, the augmenting factors for the unshaded segments of Table 1 are as follows:

Table 3 Segment multiplicative timing adjustments

	$m = 0$	$m = 1$
$n = 0$	1	1
$n = 1$	1	-0.432
$n = 2$	-0.62	-0.282

Applying these multiplicative factors to the non-shaded elements of Table 1 yields:

Table 4 Augmented forces of Table 1 and Table 3 / Newtons ($\times 10^{-8}$)

	$m = 0$	$m = 1$
$n = 0$	8.284271E-08 A	1.657607E-09 D
$n = 1$	6.155281E-09 B	-1.012499E-09 E
$n = 2$	-1.012261E-09 C	-3.324038E-10 F

For simplicity, the cells (0,0), (0,1), (0,2), (1,0), (1,1) and (1,2) above have been labeled A, B, C, D, E, and F respectively.

Then the plate force, F_p , is:

$$F_p = F_{0,0} + F_{0,1} + F_{0,2} + F_{1,0} + F_{1,1} + F_{1,2}$$

Where each $F_{m,n}$ is the sum of the six segments on the opposing plate. Then, taking account of the symmetry, $F_{\pm m, \pm n} = F_{m,n}$, the total SCAM force for the 2 x 3 example is the sum of the six components:

$$F_{0,0} = A + B + C + D + E + F = 8.829843 \times 10^{-8} \text{ I}^2$$

$$F_{0,1} = A + B + B + D + E + E = 9.478588 \times 10^{-8} \text{ I}^2$$

$$F_{0,2} = A + B + C + D + E + F = 8.829843 \times 10^{-8} \text{ I}^2$$

$$F_{1,0} = A + B + C + D + E + F = 8.829843 \times 10^{-8} \text{ I}^2$$

$$F_{1,1} = A + B + B + D + E + E = 9.478588 \times 10^{-8} \text{ I}^2$$

$$F_{1,2} = A + B + C + D + E + F = 8.829843 \times 10^{-8} \text{ I}^2$$

$$\text{Then using } F_p = F_{0,0} + F_{0,1} + F_{0,2} + F_{1,0} + F_{1,1} + F_{1,2},$$

$$F_p = 5.427655 \times 10^{-7} \text{ I}^2$$

$$\text{and the average force per segment is } \frac{5.427655 \times 10^{-7}}{6} \text{ I}^2 = 9.046091 \times 10^{-8} \text{ I}^2$$

The above analysis is applied to plates of various dimensions as shown below. The numbers show the plate dimension, M x N, the total SCAM force, and the average force per segment pair.

Table 5: Force (in Newtons) calculations for various SCAM sizes

M x N	total force ($\times \text{I}^2$)	average force per segment ($\times \text{I}^2$)
1 x 1	8.284×10^{-8}	8.284×10^{-8}
2 x 2	3.586×10^{-7}	8.964×10^{-8}
2 x 3	5.428×10^{-7}	9.046×10^{-8}
3 x 3	8.099×10^{-7}	8.998×10^{-8}
4 x 4	1.432×10^{-6}	8.949×10^{-8}
5 x 5	2.232×10^{-6}	8.929×10^{-8}
10 x 10	8.846×10^{-6}	8.846×10^{-8}
20 x 20	3.518×10^{-5}	8.795×10^{-8}
50 x 50	2.190×10^{-4}	8.761×10^{-8}
100 x 100	8.749×10^{-4}	8.749×10^{-8}

These numbers were calculated using a computer program. The 100 x 100 case took just over 27 hours to complete. For this reason, forces for $M, N > 100$ were not calculated. However, it can be seen from the averages that for large SCAM size, the average force per segment, F_s , is approximately $8.7 \times 10^{-8} I^2$ Newtons.

This force is further augmented by the 1/3 temporal pulse used as the segment current, (FIGS 1 and 2) thus reducing the effective force by a factor of 3:

$$F_s \approx 8.7 \times 10^{-8} / 3 I^2 \text{ Newtons}$$

$$F_s \approx 2.9 \times 10^{-8} I^2 \text{ Newtons}$$

Example SCAM applying the above force to plates of 1000 x 1000 segments carrying 100 Amps:

$$M = N = 1000$$

$$I = 100 \text{ Amps}$$

$$\text{SCAM force } F_p = M \times N \times F_s \times I \times I \text{ Newtons}$$

$$\text{SCAM force } F_p = 1000 \times 1000 \times 2.9 \times 10^{-8} \times 100 \times 100 = 290 \text{ N}$$

As technology advances, it will become possible to build SCAMs of higher and higher frequency, facilitating a smaller separation, a , and larger M and N values. Similarly, as superconductor technology advances, SCAMs will be able operate at higher currents.

Consider a case where $M = N = 100000$ and $I = 1000$ Amps, then using

$$\text{SCAM force } F_p = M \times N \times F_s \times I \times I \text{ Newtons}$$

$$\text{SCAM force } F_p = 100000 \times 100000 \times 2.9 \times 10^{-8} \times 1000 \times 1000 = 290,000,000 \text{ N}$$